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# $CO<sub>2</sub>$  reforming of CH<sub>4</sub> in coke oven gas to syngas over coal char catalyst

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#### **ABSTRACT**

The CO2 reforming of methane (in coke oven gas) on the coal char catalyst was performed in a fixed bed reactor at temperatures between 800 and 1200 ℃ under normal pressure. The effects of the coal char catalyst pretreatment and the ratio of  $CO<sub>2</sub>/CH<sub>4</sub>$  were studied. Experimental results showed that the coal char was an effective catalyst for production of syngas, and addition of  $CO<sub>2</sub>$  did not enhance the CH<sub>4</sub> reforming to H<sub>2</sub>. It was also found that the product gas ratio of H<sub>2</sub>/CO is strongly influenced by the feed ratio of  $CO<sub>2</sub>/CH<sub>4</sub>$ . The modified coal char catalyst was more active during the  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming than the coal char catalyst based on the catalyst volume, furthermore the modified catalyst exhibited high activity in  $CO<sub>2</sub>-CH<sub>4</sub>$  reforming to syngas. The conversion of methane can be divided into two stages. In the first stage, the conversion of  $CH_4$  gradually decreased. In the second stage, the conversion of methane maintained nearly constant. The conversion of  $CO<sub>2</sub>$  decreased slightly during the overall reactions in  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming. The coal char catalyst is a highly promising catalyst for the  $CO<sub>2</sub>$  reforming of methane to syngas.

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# **1. Introduction**

The methane reforming process, for example  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming, produces synthetic gas that is the main route to convert methane to liquid fuels, ammonia, methanol, and other oxygenates in so-called gas to liquid (GTL) technologies [\[1–3\].](#page-3-0) The conversion of the two gases into a valuable synthesis gas would reduce emissions of  $CO<sub>2</sub>$  and  $CH<sub>4</sub>$  and also satisfy the requirement of many synthesis processes in the chemical industry. Furthermore, it has potential in the co-utilisation of coke oven gas and coal bed methane  $[3-5]$ . In view of these advantages, it is likely that  $CO<sub>2</sub>$ reforming of methane will become increasingly important in the future. With temperature range from 800 to 1200 $\degree$ C, numerous supported catalysts studies on  $CO<sub>2</sub>$  reforming have been tested in fixed and fluidized bed reactors, especially nickel- and noble metalbased catalysts [\[6\]. A](#page-4-0)lthough noble metals are more active, selective for  $CO<sub>2</sub>$  reforming and less sensitive to coking than Ni-based catalysts, but considering the high cost and limited availability of noble metals, these have discouraged their industrial application [\[7,8\]. F](#page-4-0)rom the industrial standpoint, Ni-based catalysts have been employed as possible substitutes for precious metals as they are relatively cheap and exhibit high activity for the reaction [\[7,8\].](#page-4-0)

However, the problem of  $CO<sub>2</sub>-CH<sub>4</sub>$  reforming is carbon deposition on the nickel catalysts surface and cause the catalyst deactivation. Therefore, the search for suitable new catalysts is still a research priority. A possible alternative and a new kind of cheap catalyst is coal char, which has been reported to have significant potential [\[3,9,10\].](#page-3-0)

Very recently, coal char as a highly promising catalyst for the carbon-free  $H_2O$  reforming of methane (in coke oven gas) has been reported [\[9,10\]. T](#page-4-0)his catalyst showed not only a high resistance to carbon formation, but also a high activity and selectivity in the  $H_2O$ reforming. In the present work, the  $CO<sub>2</sub>$  reforming of methane over the coal char catalyst at different process conditions (viz. reaction temperature and relative concentrations of methane and  $CO<sub>2</sub>$  in the feed) will be discussed.

#### **2. Experimental**

Three different catalysts composed of coal char were used in the experiment. The coal char catalysts were prepared by pyrolysis of coal at 1150 °C for 1.5 h, crushing the catalyst mass to 30–60 mesh-size particles. The modified catalyst was prepared by the impregnation method in a stirred sodium hydroxide aqueous solution at normal temperature for 3 h. The modified catalyst was dried in a drying oven for 12 h at 100 $^{\circ}$ C. The composition of the catalyst is provided in [Table 1. T](#page-1-0)he composition of coke oven gas used in the experiment was shown in [Table 2.](#page-1-0)

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<span id="page-1-0"></span>



#### **Table 2**

The composition of coke oven gas.



The catalytic reforming reactions of  $CH<sub>4</sub>-CO<sub>2</sub>$  over the catalyst were carried out at normal pressure in a continuous-flow quartz reactor (i.d. 20 mm) packed with 0.4–1.1 g catalyst and provided with a platinum–rhodium thermocouple located in the center of the catalyst bed. Before carrying out the reaction, the catalyst was heated in situ at 800 °C in a flow (50 cm<sup>3</sup> min<sup>-1</sup>) of moisture-free nitrogen for 1 h.

The catalytic reactions were carried out at different temperatures, and relative concentrations of  $CH_4$ ,  $H_2$ ,  $CO_2$  in the feed were measured, at normal temperature and pressure. The feed gases and the product gases were analyzed by gas chromatography −960. The methane (in coke oven gas) intake can be measured by mass flow meter. And the output of product gas flow can be measured by soap liquid meter. The C, H, and O balance across the reactor was more than 97%. All experiments with larger errors in the material balances were rejected. The formula of  $H_2$ , CO, and CH<sub>4</sub> relative volume (to  $CH_4$  in feed gas),  $CH_4$  and  $CO_2$  conversion, which were

Relative Volume( $H_2$  or CO)

$$
= \frac{\text{Content in production gas} - \text{Content in feed}}{\text{Content of CH}_4 \text{ in feed}}
$$
\n
$$
Relative Volume(CH_4) = \frac{\text{Content in feed} - \text{Content in production gas}}{\text{Content of CH}_4 \text{ in feed}}
$$
\n
$$
conversion(CH_4) = \frac{\text{Content in feed} - \text{Content in production gas}}{\text{Content of CH}_4 \text{ in feed}}
$$
\n
$$
conversion(CO_2) = \frac{\text{Content in feed} - \text{Content in production gas}}{\text{Content of CO}_2 \text{ in feed}}
$$

## **3. Results and discussion**

*3.1. Effects of coal char catalyst on CH4 (in coke oven gas) pyrolysis and CO2–CH4 reformation*

Fig. 1 shows the CH<sub>4</sub> pyrolysis and CO<sub>2</sub>–CH<sub>4</sub> reforming conversion change during the reactions at different temperature. It also can be seen obviously that the coal char had apparent catalyzation to  $CH<sub>4</sub>$  (in coke oven gas) pyrolysis in the temperature range from 800 to 1200  $\degree$ C. Compared with blank test, CH<sub>4</sub> pyrolysis takes place at 950 $\degree$ C with coal char catalyst and has more CH<sub>4</sub> conversion during pyrolysis. With the reaction temperature increasing, the conversion of CH4 gradually increases. When the reaction temperature arrived at 1050 $\degree$ C, the conversion of CH<sub>4</sub> is about 50% with coal char catalyst, and the conversion of  $CH<sub>4</sub>$  is about 35% without coal char catalyst. The data shows that the coal char could promote some of CH<sub>4</sub> conversion.

Based on the data of experiment as Fig. 1, it could be also concluded that the coal char had apparent catalyzation to  $CO<sub>2</sub> - CH<sub>4</sub>$ 



**Fig. 1.** Conversion change of overall reactions in CH<sub>4</sub>-CO<sub>2</sub> reforming or CH4 pyrolysis (reaction condition: catalysts: coal char catalyst II or quartz powder catalyst, residence time: 3 s,  $CO_2/CH_4 \approx 1:1$ ,  $CO_2:12$  mL/min, coke oven gas: 50 mL/min).

(in coke oven gas) reforming in the temperature range from 800 to 1200 °C. During reforming of  $CO<sub>2</sub>$ –CH<sub>4</sub> the following reaction may take place

$$
CH_4 \to C + 2H_2 \tag{1}
$$

$$
CH_4+2CO_2 \rightarrow 2CO + 2H_2 \tag{2}
$$

Addition of  $CO<sub>2</sub>$  does not enhance the CH<sub>4</sub> reforming to H<sub>2</sub>, because of a great amount of  $H_2$  in feed (coke oven gas). This indicates, under  $H_2$  atmosphere, adding  $CO<sub>2</sub>$  is disadvantageous to the transformation of  $CH<sub>4</sub>$  during reforming process.

#### *3.2. Effects of temperature on distribution of the product gas*

The  $CO<sub>2</sub>$  reforming of methane (in coke oven gas) was carried out by passing a mixture of  $CO<sub>2</sub>$  and CH<sub>4</sub> (in coke oven gas) over coal char catalyst, while keeping  $CO<sub>2</sub>/CH<sub>4</sub>$  ratio (1.0) constant in the feed, under the temperature range from 700 to 1200 ℃. Results showing the influence of temperature on the conversion and product gas relative content are presented in [Fig. 2. I](#page-2-0)t can be found that the relative content of  $CH<sub>4</sub>$  nearly unchanged when the reforming temperature is below 900 $\degree$ C. However, from Fig. 1, it can be seen obviously that  $H_2$  and  $CO_2$  are consumed, and CO are formed. It can be interpreted as follows:

$$
CO_4 + H_2 \rightarrow H_2O + CO \tag{3}
$$

$$
C + CO_2 \rightarrow 2CO \tag{4}
$$

After the produce gas was condensated, a slight amount of water was found, which indicated the reaction (3) had taken place.

When the reforming temperature is higher than 1065 ◦C, the conversion of  $CO<sub>2</sub>$  was basically 100%, the relative volume of  $H<sub>2</sub>$ 

<span id="page-2-0"></span>

**Fig. 2.** The distribution diagram of production gas in the experiment of  $CO<sub>2</sub>/CH<sub>4</sub>$  reforming (reaction condition: coal char catalyst II, residence time: 3 s,  $CO_2:CH_4 \approx 1:1$ ,  $CO_2:12$  mL/min, coke oven gas:50 mL/min, the relative volume of  $CH<sub>4</sub>$ , H<sub>2</sub> and CO is to CH<sub>4</sub> in feed gas).

reached more than 200%. In the  $CO<sub>2</sub>$ -methane reforming process, both the  $CO<sub>2</sub>$  and  $H<sub>2</sub>O$  may be converted simultaneously by the reactions as follow[s\[9\]:](#page-4-0)

$$
CH4 + CO2 \rightarrow 2CO + 2H2 - 247.39 \text{ kJ/mol}
$$
  
\n
$$
\Delta G0 = 61770 - 67.32T
$$
\n(5)

$$
CH4 + H2O → CO + 3H2 – 206.37 kJ/mol
$$
  
ΔG<sup>0</sup> = 189982 – 142.09T (6)

The  $CO<sub>2</sub>$  reforming of methane (in coke oven gas) was studied over quartz powder, while keeping  $CO<sub>2</sub>/CH<sub>4</sub>$  ratio (1.0) constant in the feed under the temperature range from 900 to 1200 ℃. The results as Fig. 3 shown, there is almost no influence on the CH4



**Fig. 3.** The distribution diagram of production gas in the experiment of  $CO<sub>2</sub>/CH<sub>4</sub>$ reforming (reaction condition: Quartz powder, residence time: 3 s,  $CO_2:CH_4 \approx 1:1$ ,  $CO_2$ :12 mL/min, coke oven gas: 50 mL/min, the relative volume of CH<sub>4</sub>, H<sub>2</sub> and CO is to CH<sub>4</sub> in feed gas).

conversion when the reforming temperature is below 1000 ◦C, but  $H<sub>2</sub>$  and CO<sub>2</sub> consumed, which could be explained by reactions [\(3\)](#page-1-0) and [\(4\). T](#page-1-0)he  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming reaction begin about 1000 °C over quartz powder, CO and  $H_2$  are produced.

When the reforming temperature arrived at 1050 °C, the results show that the formation rate of  $H_2$  is far higher than its consumption rate, which indicates that reactions (5) and (6) play a leading position at the latter stage (1065–1200 ◦C). At 1200 ◦C, the conversion of  $CO<sub>2</sub>$  seems complete. The higher temperature is favored to  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming reaction. Compared the distribution diagram of production gas of  $CO<sub>2</sub>-CH<sub>4</sub>$  reforming over coal char catalyst with quartz powder, it can be seen that the starting reaction temperature differences compared with quartz powder is lower than about 100 $\degree$ C for coal char catalyst.

#### *3.3. Effects of different coal char catalyst on CO2–CH4 reformation*

To investigate the effect of different coal char catalyst on  $CO<sub>2</sub>$ reforming of methane, several experiments were conducted, both in the presence and absence of the char catalyst and the results are presented in Fig. 4. It can be seen that the methane conversion both over the quartz powder and catalyst II is about 10%, furthermore, the methane conversion over catalyst I is about 30% at temperature 1000 $\degree$ C. At the same temperature, the conversion over catalyst III is some 50%. Clearly, the catalyst III displayed a significant higher catalytic activity than catalyst I and II, catalytic activity sequence of the catalysts is catalyst  $III > I > II$ .

The temperature has an evident influence on catalytic activity. The catalyst III has higher catalytic activity at the temperature 950 °C, however catalytic activity is very weak for catalyst I and II. Fig. 4 also shows the negligible difference in performance of catalyst I and II before 1000 ◦C. After temperatures above reaching 1050 $\degree$ C, the acivty of catalyst I is much higher than catalyst II. After temperature reaching 1100 $\degree$ C, there is no discernable difference between coal char catalyst I and III. At higher temperature 1200 $\degree$ C, the catalytic activity of three kinds of catalyst is same. This suggests that different coal char materials have an evident influence on  $CH_4$ - $CO_2$  reforming reaction at different temperature.



Fig. 4. CH<sub>4</sub> Conversion in CH<sub>4</sub>–CO<sub>2</sub> Reforming Catalyzed by Different Coal char Catalyst (reaction condition: different coal char catalyst, residence time: 3 s,  $CO_2:CH_4 \approx 1:1$ ,  $CO_2:12$  mL/min, coke oven gas: 50 mL/min).

<span id="page-3-0"></span>

**Fig. 5.** Effect of  $CO_2$ /CH<sub>4</sub> ratio on  $CO/H_2$  ratio in the  $CO_2$  reforming of methane over coal char catalyst (reaction condition: coal char Catalyst II, temperature: 1050 ◦C, coke oven gas:50 mL/min).

### *3.4. Effects of CO2/CH4 ratio on the rate of CO/H2 in produce gas*

The influence of  $CO<sub>2</sub>/CH<sub>4</sub>$  feed ratio on the catalyst performance in the  $CO<sub>2</sub>$  reforming of methane was also studied at temperatures 1050 °C over coal char Catalyst II. The results (Fig. 5) show a strong influence of the  $CO<sub>2</sub>/CH<sub>4</sub>$  feed ratio on the process performance. With the  $CO_2/CH_4$  feed ratio increasing, the  $CO/H_2$  ratio is also increased. When the feed ratio of  $CO<sub>2</sub>/CH<sub>4</sub>$  arrived at 1:1, the conversion of CH<sub>4</sub> was about 97.35%, the ratio of CO/H<sub>2</sub> is about 1:3 in produce gas. While the feed ratio of  $CO<sub>2</sub>/CH<sub>4</sub>$  arrived at 2:1, the CO/H<sub>2</sub> ratio is approximately 1:1.1. Hence, the CO/H<sub>2</sub> ratio of  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming could be adjusted by means of adjusting the feed ratio of  $CO<sub>2</sub>/CH<sub>4</sub>$ .

# *3.5. Reaction activity and life of catalyst*

The life of catalyst of the  $CO<sub>2</sub>$  reforming of  $CH<sub>4</sub>$  was shown in Fig. 6. It can be found that the conversion of methane can be divided into two stages. In the first stage, the conversion of  $CH<sub>4</sub>$  is about 95.2% at the beginning, then with the reaction time extend, the



**Fig. 6.** The life of the coal char catalyst during  $CO<sub>2</sub>/CH<sub>4</sub>$  reforming (reaction condition: coal char catalyst III, temperature:950 °C,  $\text{CO}_2$ :CH<sub>4</sub>  $\approx$  1:1,  $\text{CO}_2$ :12 mL/min, coke oven gas:50 mL/min).

#### **Table 3**

The change of oxygen-bearing functional group in c-catalyst.

Item	The content of oxygen-bearing functional group (%)				
	$C-C$	Phenolic hydroxyl Carbonyl		Carboxyl	Lactone
Before reaction After reaction	56.60 82.14	28.66 4.20	6.08 979	6.04 3.67	2.62 0.20

conversion of  $CH<sub>4</sub>$  obviously decreases, reaches the lowest at 210 mins, about 38.3%. Then the second stage, the conversion of CH4 maintain nearly constant, about 40%.

Through X-ray photoelectron spectra, four oxygen-bearing functional group can be detected on the surface of catalyst: phenolic hydroxyl, carbonyl, carboxyl and lactone. The content of oxygenbearing functional group in catalyst is shown in Table 3.

It can be found from Table 3, after  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming, the content of oxygen-bearing functional group in catalyst declined fiercely, especially the phenolic hydroxyl and lactone, decreases from 28.66% and 2.62% to 4.2% and 0.2%, respectively. Based on the phenomenon mentioned above, it can be concluded that the phenolic hydroxyl and lactone play an important role in  $CO<sub>2</sub>$ –CH<sub>4</sub> reforming, and promote the conversion of  $CH<sub>4</sub>$  efficiently. However, with the phenolic hydroxyl and lactone consuming, the conversion of  $CH<sub>4</sub>$  drop off. When the phenolic hydroxyl and lactone is consumed completely, the conversion of methane maintains nearly constant.

It also can be seen from Fig. 6, the tendency of carbon dioxide conversion is different from methane, the conversion of  $CO<sub>2</sub>$ decreases slightly during the overall  $CO<sub>2</sub>-CH<sub>4</sub>$  reforming reactions. This indicates that the coal char catalyst during reforming process has high activity for  $CO_2$ , and better catalyst stability for  $CO_2$ -CH<sub>4</sub> reforming at 200 min later, which is promising new catalyst for transforming coke oven gas to syngas.

#### **4. Conclusions**

The coal char catalyst is a highly promising catalyst for the  $CO<sub>2</sub>$ reforming of methane to syngas. The  $CO/H<sub>2</sub>$  ratio in the  $CO<sub>2</sub>$  reforming of methane can be adjusted by means of adjusting by feed ratio of  $CO<sub>2</sub>/CH<sub>4</sub>$ , which rang from 0.2 to 1.1. The modified coal char catalyst has more active than coal char catalyst I and II in  $CO<sub>2</sub>$ reforming of CH4. For the modified coal char catalyst, the conversion of methane can be divided into two stages. In the first stage, with the reaction time extend, the conversion of  $CH<sub>4</sub>$  gradually decreases. In the second stage, the conversion of methane maintains nearly constant. The conversion of  $CO<sub>2</sub>$  decreases slightly during the overall  $CH<sub>4</sub>$ - CO<sub>2</sub> reforming reactions.

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